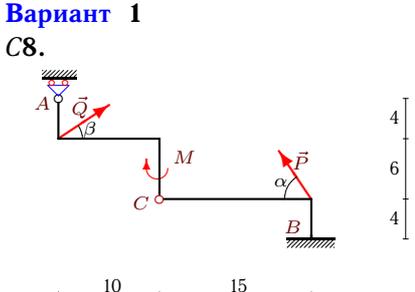
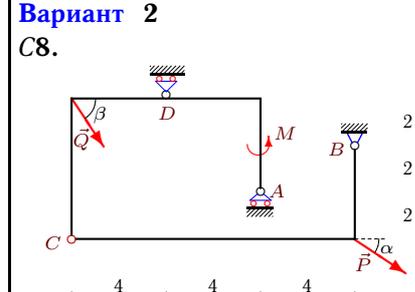
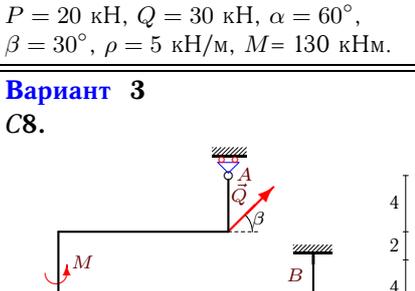
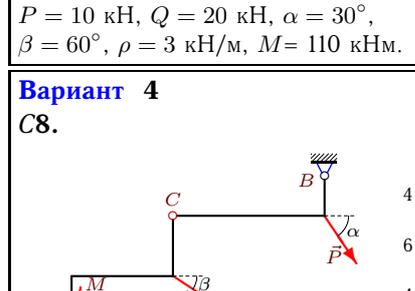
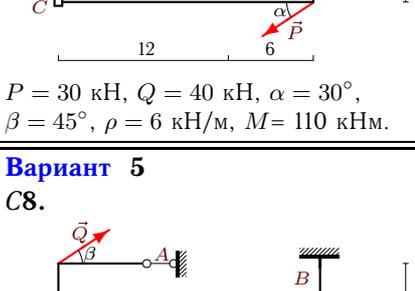
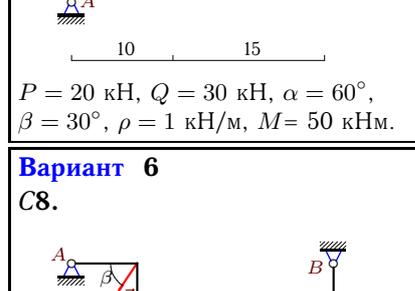
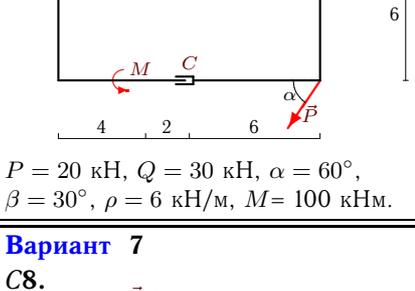
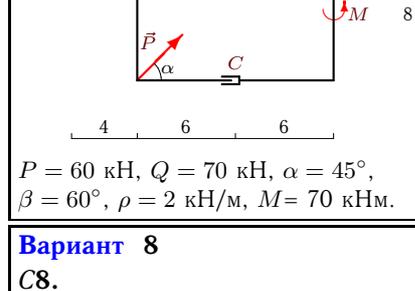
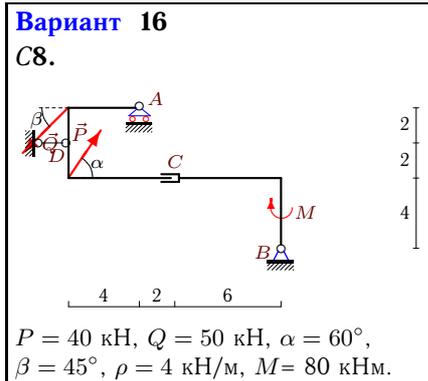
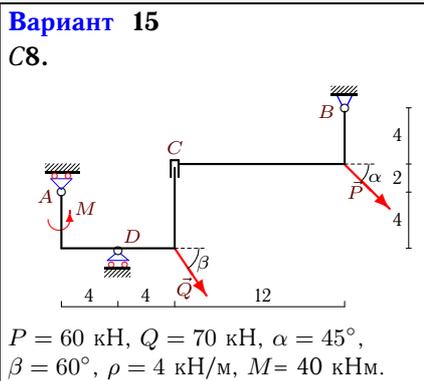
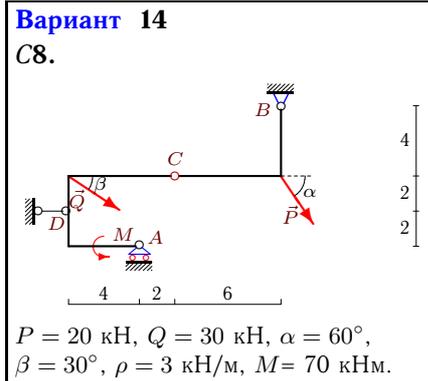
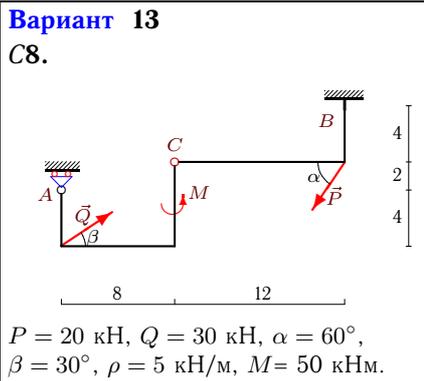
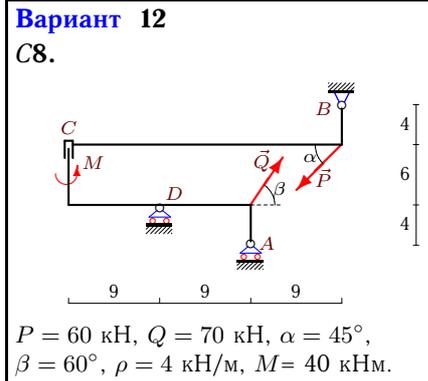
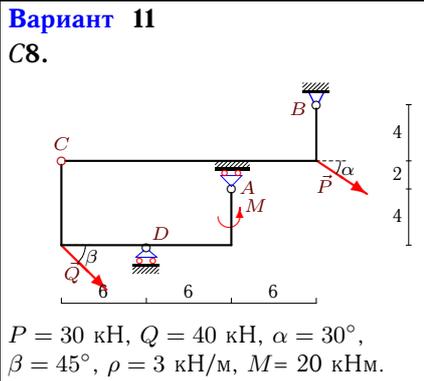
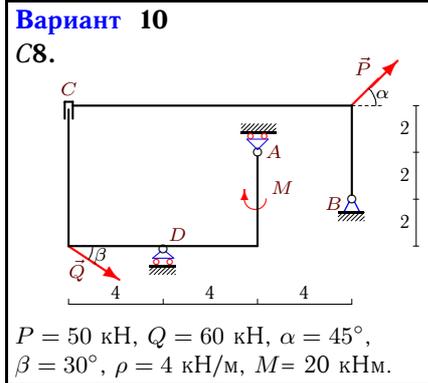
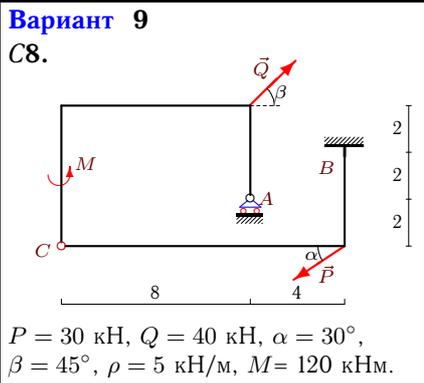


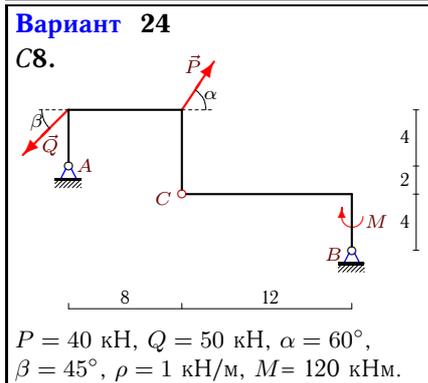
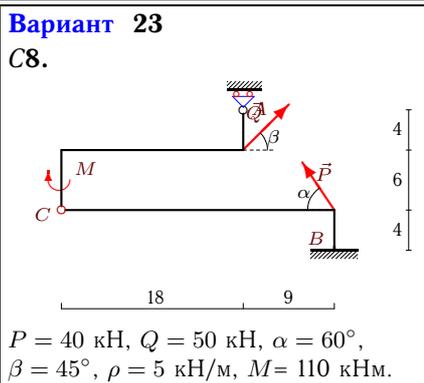
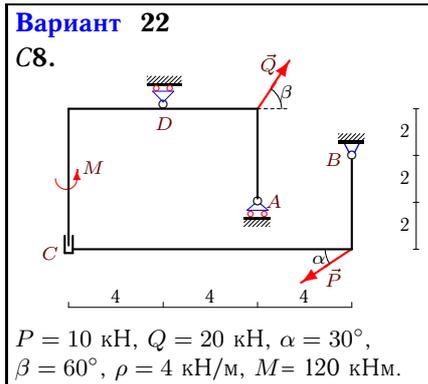
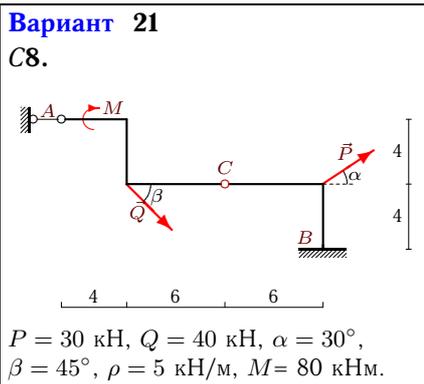
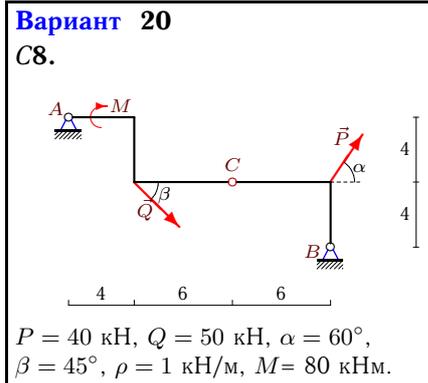
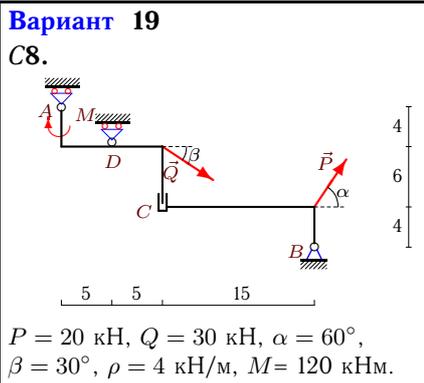
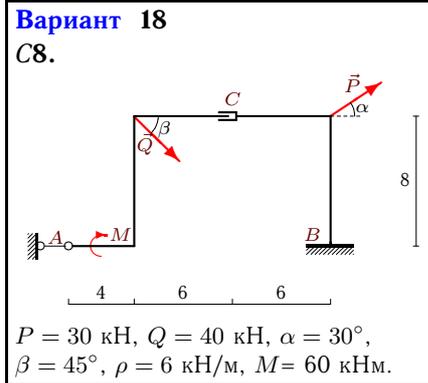
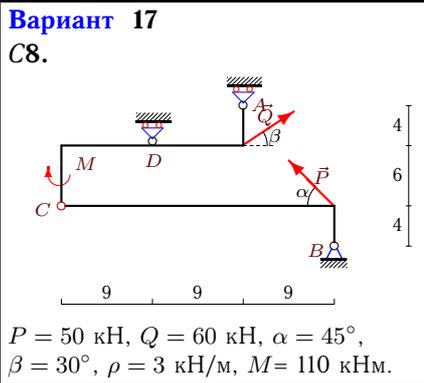
Расчет составной конструкции

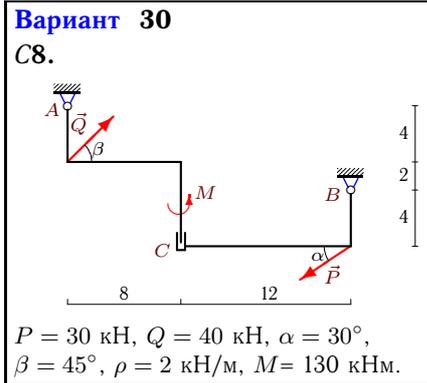
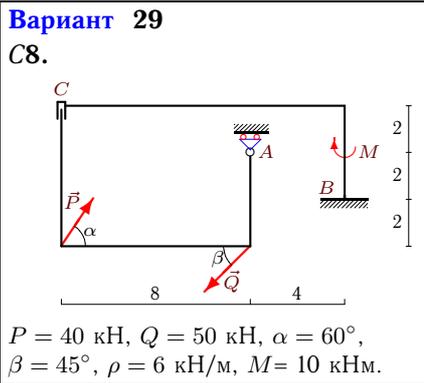
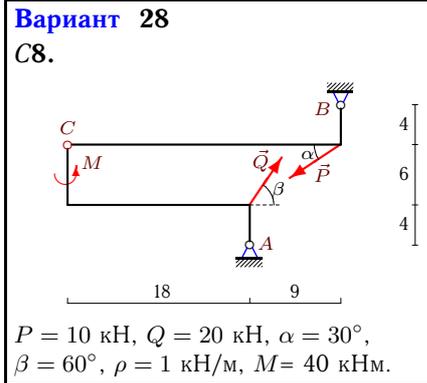
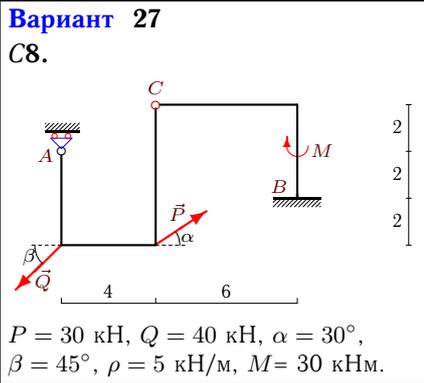
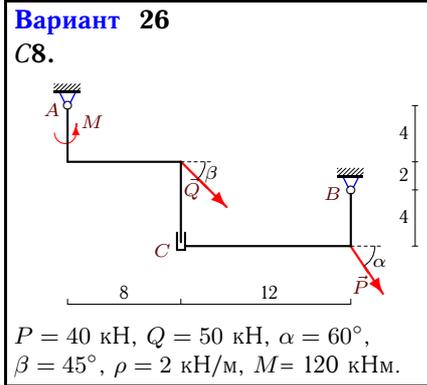
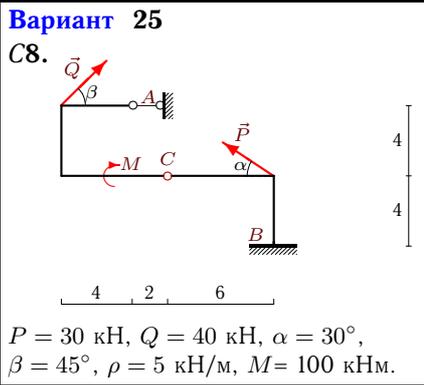
Рама состоит из двух частей, соединенных шарниром или скользящей заделкой. Дан погонный вес рамы ρ , размеры в метрах и нагрузки. Найти реакции опор.

Кирсанов М.Н. Решебник. Теоретическая механика с. 54.

<p>Вариант 1 С8.</p>  <p>$P = 20 \text{ кН}, Q = 30 \text{ кН}, \alpha = 60^\circ,$ $\beta = 30^\circ, \rho = 5 \text{ кН/м}, M = 130 \text{ кНм}.$</p>	<p>Вариант 2 С8.</p>  <p>$P = 10 \text{ кН}, Q = 20 \text{ кН}, \alpha = 30^\circ,$ $\beta = 60^\circ, \rho = 3 \text{ кН/м}, M = 110 \text{ кНм}.$</p>
<p>Вариант 3 С8.</p>  <p>$P = 30 \text{ кН}, Q = 40 \text{ кН}, \alpha = 30^\circ,$ $\beta = 45^\circ, \rho = 6 \text{ кН/м}, M = 110 \text{ кНм}.$</p>	<p>Вариант 4 С8.</p>  <p>$P = 20 \text{ кН}, Q = 30 \text{ кН}, \alpha = 60^\circ,$ $\beta = 30^\circ, \rho = 1 \text{ кН/м}, M = 50 \text{ кНм}.$</p>
<p>Вариант 5 С8.</p>  <p>$P = 20 \text{ кН}, Q = 30 \text{ кН}, \alpha = 60^\circ,$ $\beta = 30^\circ, \rho = 6 \text{ кН/м}, M = 100 \text{ кНм}.$</p>	<p>Вариант 6 С8.</p>  <p>$P = 60 \text{ кН}, Q = 70 \text{ кН}, \alpha = 45^\circ,$ $\beta = 60^\circ, \rho = 2 \text{ кН/м}, M = 70 \text{ кНм}.$</p>
<p>Вариант 7 С8.</p>  <p>$P = 40 \text{ кН}, Q = 50 \text{ кН}, \alpha = 60^\circ,$ $\beta = 45^\circ, \rho = 1 \text{ кН/м}, M = 50 \text{ кНм}.$</p>	<p>Вариант 8 С8.</p>  <p>$P = 10 \text{ кН}, Q = 20 \text{ кН}, \alpha = 30^\circ,$ $\beta = 60^\circ, \rho = 1 \text{ кН/м}, M = 60 \text{ кНм}.$</p>







Ответы

	X_A	Y_A	X_B	Y_B	X_D	Y_D	M_B
1	—	1.41	-15.98	161.27	—	—	-1752.4
2	—	-60.04	-18.66	28.78	—	155.58	—
3	—	103.72	-2.3	147	—	—	-1785.5
4	30.7	60.28	-66.67	11.04	—	—	—
5	-25.98	—	10	170.32	—	—	-964
6	-7.43	67.23	0	14.96	—	—	—
7	24.33	1.41	-8.98	31.3	—	—	—
8	-4.83	27.49	6.17	12.83	—	—	—
9	—	17.93	-2.3	138.79	—	—	-894.66
10	—	-95.63	-87.32	28.64	—	197.63	—
11	—	-104.96	-54.27	41.94	—	238.3	—
12	—	-255.1	7.43	166.43	—	306.48	—
13	—	50.74	-15.98	121.58	—	—	-715.1
14	—	-64.04	195.06	168.36	-231.04	—	—
15	—	143.3	-77.43	106.43	—	-10.68	—
16	—	84.91	0	11.8	15.36	—	—
17	—	-27.18	-16.6	19.6	—	119.22	—
18	-28.28	—	-25.98	205.28	—	—	-1189.3
19	—	-16.96	-35.98	58.68	—	111.96	—
20	-19.36	28.36	-36	-3.64	—	—	—
21	114.93	—	-169.2	133.28	—	—	-2.94
22	—	-113.66	-1.34	69	—	168.34	—
23	—	47.54	-15.36	177.46	—	—	-3302.88
24	-420.47	159.99	435.82	-125.27	—	—	—
25	-23.21	—	20.9	76.72	—	—	-423.92
26	-28.26	71.36	-27.1	66.64	—	—	—
27	—	54.83	2.3	78.46	—	—	-239.95
28	-48.68	17.17	47.34	29.51	—	—	—
29	—	108.71	15.36	96	—	—	-594.16
30	-7.75	7.72	5.45	47	—	—	—