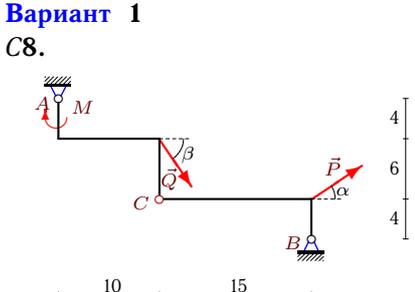
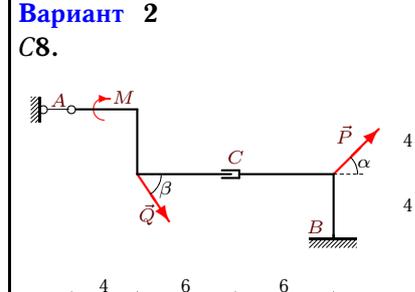
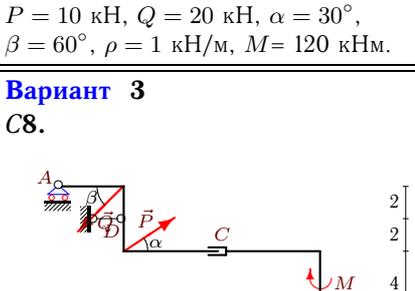
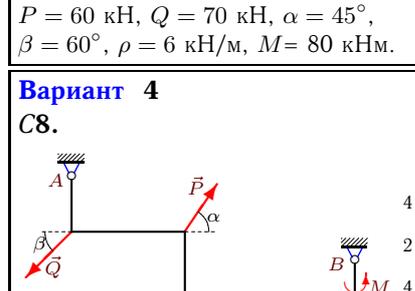
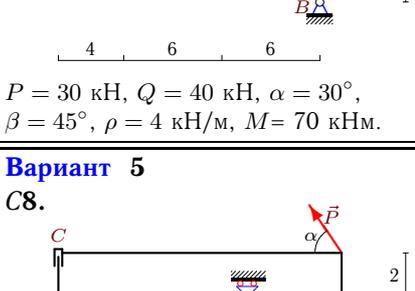
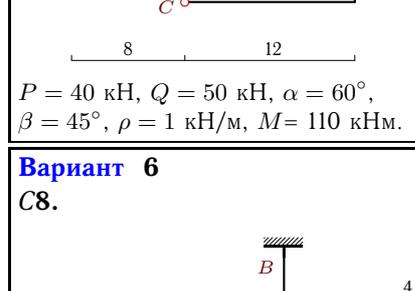
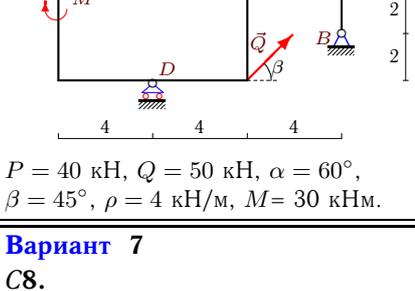
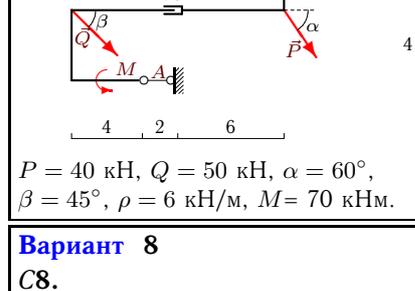


## Расчет составной конструкции

Рама состоит из двух частей, соединенных шарниром или скользящей заделкой. Дан погонный вес рамы  $\rho$ , размеры в метрах и нагрузки. Найти реакции опор.

*Кирсанов М.Н. Решебник. Теоретическая механика с. 54.*

<p><b>Вариант 1</b> С8.</p>  <p><math>P = 10 \text{ кН}, Q = 20 \text{ кН}, \alpha = 30^\circ,</math> <math>\beta = 60^\circ, \rho = 1 \text{ кН/м}, M = 120 \text{ кНм}.</math></p>	<p><b>Вариант 2</b> С8.</p>  <p><math>P = 60 \text{ кН}, Q = 70 \text{ кН}, \alpha = 45^\circ,</math> <math>\beta = 60^\circ, \rho = 6 \text{ кН/м}, M = 80 \text{ кНм}.</math></p>
<p><b>Вариант 3</b> С8.</p>  <p><math>P = 30 \text{ кН}, Q = 40 \text{ кН}, \alpha = 30^\circ,</math> <math>\beta = 45^\circ, \rho = 4 \text{ кН/м}, M = 70 \text{ кНм}.</math></p>	<p><b>Вариант 4</b> С8.</p>  <p><math>P = 40 \text{ кН}, Q = 50 \text{ кН}, \alpha = 60^\circ,</math> <math>\beta = 45^\circ, \rho = 1 \text{ кН/м}, M = 110 \text{ кНм}.</math></p>
<p><b>Вариант 5</b> С8.</p>  <p><math>P = 40 \text{ кН}, Q = 50 \text{ кН}, \alpha = 60^\circ,</math> <math>\beta = 45^\circ, \rho = 4 \text{ кН/м}, M = 30 \text{ кНм}.</math></p>	<p><b>Вариант 6</b> С8.</p>  <p><math>P = 40 \text{ кН}, Q = 50 \text{ кН}, \alpha = 60^\circ,</math> <math>\beta = 45^\circ, \rho = 6 \text{ кН/м}, M = 70 \text{ кНм}.</math></p>
<p><b>Вариант 7</b> С8.</p>  <p><math>P = 10 \text{ кН}, Q = 20 \text{ кН}, \alpha = 30^\circ,</math> <math>\beta = 60^\circ, \rho = 6 \text{ кН/м}, M = 40 \text{ кНм}.</math></p>	<p><b>Вариант 8</b> С8.</p>  <p><math>P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,</math> <math>\beta = 30^\circ, \rho = 6 \text{ кН/м}, M = 70 \text{ кНм}.</math></p>

**Вариант 9**  
С8.

$P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 30^\circ, \rho = 1 \text{ кН/м}, M = 80 \text{ кНм}.$

**Вариант 10**  
С8.

$P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 30^\circ, \rho = 3 \text{ кН/м}, M = 20 \text{ кНм}.$

**Вариант 11**  
С8.

$P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 30^\circ, \rho = 2 \text{ кН/м}, M = 50 \text{ кНм}.$

**Вариант 12**  
С8.

$P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 30^\circ, \rho = 5 \text{ кН/м}, M = 90 \text{ кНм}.$

**Вариант 13**  
С8.

$P = 60 \text{ кН}, Q = 70 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 60^\circ, \rho = 4 \text{ кН/м}, M = 70 \text{ кНм}.$

**Вариант 14**  
С8.

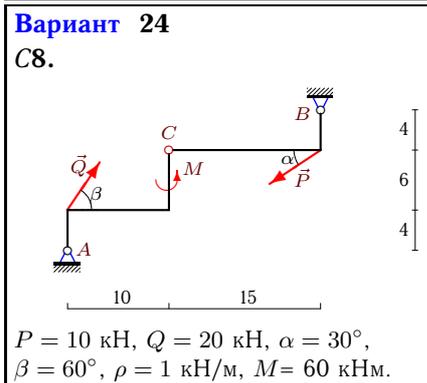
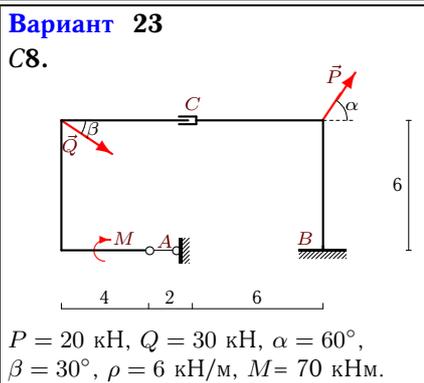
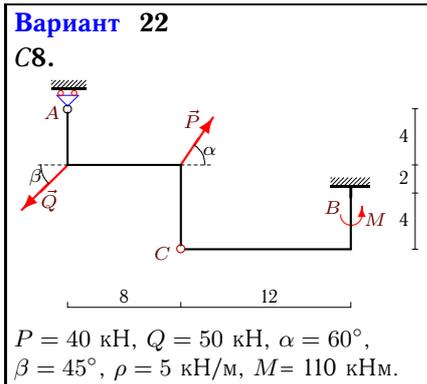
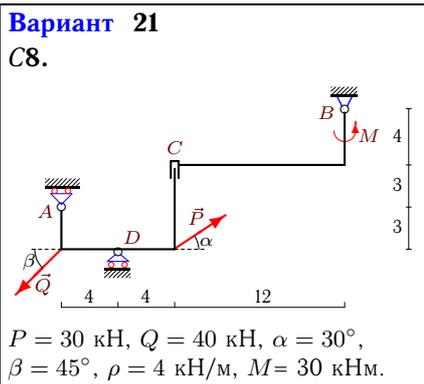
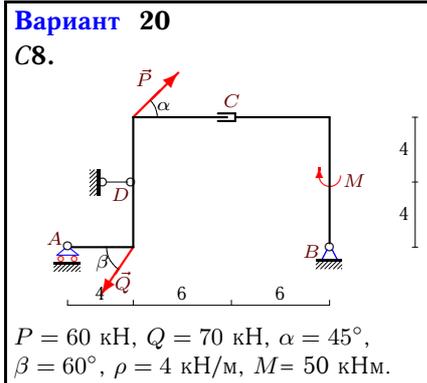
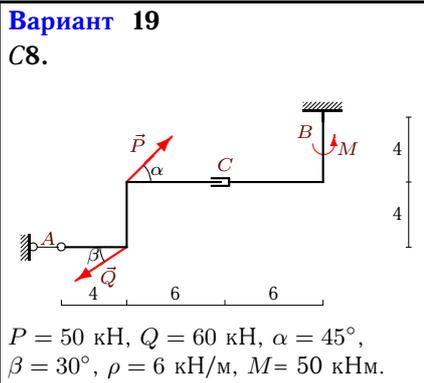
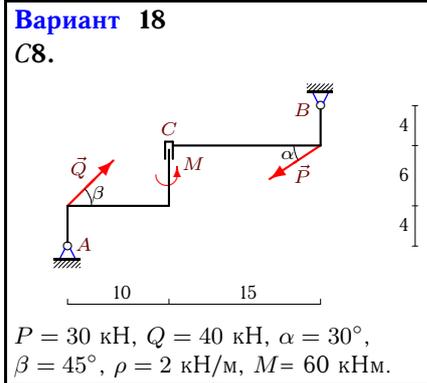
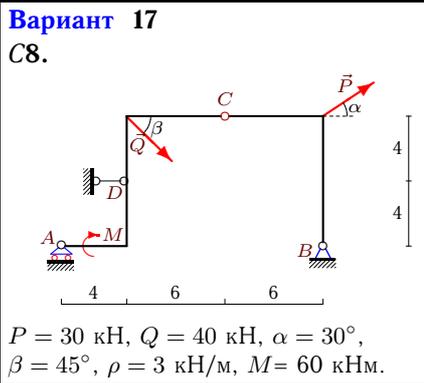
$P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 30^\circ, \rho = 5 \text{ кН/м}, M = 80 \text{ кНм}.$

**Вариант 15**  
С8.

$P = 10 \text{ кН}, Q = 20 \text{ кН}, \alpha = 30^\circ,$   
 $\beta = 60^\circ, \rho = 5 \text{ кН/м}, M = 130 \text{ кНм}.$

**Вариант 16**  
С8.

$P = 20 \text{ кН}, Q = 30 \text{ кН}, \alpha = 60^\circ,$   
 $\beta = 30^\circ, \rho = 5 \text{ кН/м}, M = 120 \text{ кНм}.$



**Вариант 25**  
С8.

$P = 60 \text{ кН}, Q = 70 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 60^\circ, \rho = 2 \text{ кН/м}, M = 70 \text{ кНм}.$

**Вариант 26**  
С8.

$P = 10 \text{ кН}, Q = 20 \text{ кН}, \alpha = 30^\circ,$   
 $\beta = 60^\circ, \rho = 3 \text{ кН/м}, M = 70 \text{ кНм}.$

**Вариант 27**  
С8.

$P = 60 \text{ кН}, Q = 70 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 60^\circ, \rho = 4 \text{ кН/м}, M = 90 \text{ кНм}.$

**Вариант 28**  
С8.

$P = 50 \text{ кН}, Q = 60 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 30^\circ, \rho = 4 \text{ кН/м}, M = 70 \text{ кНм}.$

**Вариант 29**  
С8.

$P = 60 \text{ кН}, Q = 70 \text{ кН}, \alpha = 45^\circ,$   
 $\beta = 60^\circ, \rho = 2 \text{ кН/м}, M = 70 \text{ кНм}.$

**Вариант 30**  
С8.

$P = 40 \text{ кН}, Q = 50 \text{ кН}, \alpha = 60^\circ,$   
 $\beta = 45^\circ, \rho = 1 \text{ кН/м}, M = 10 \text{ кНм}.$

Ответы

	$X_A$	$Y_A$	$X_B$	$Y_B$	$X_D$	$Y_D$	$M_B$
1	-66.6	57.6	47.95	-6.29	—	—	—
2	-35	—	-42.43	162.2	—	—	-1673.76
3	—	56.37	0	52.91	2.3	—	—
4	16.5	34.26	-1.13	0.46	—	—	—
5	—	-145.53	-15.36	29.36	—	182.18	—
6	-35.36	—	-20	214	—	—	-1392.84
7	—	120.32	1.34	96	—	—	50.68
8	-51.96	—	35.36	126.64	—	—	-1196.84
9	-63.64	-44.36	47.03	73.71	—	—	—
10	—	46.38	16.6	36.42	—	43.84	—
11	-68.7	6	52.1	67.36	—	—	—
12	-26.96	—	10.36	54.64	—	—	-371.42
13	—	129.24	-42.43	0.96	-35	—	—
14	93.75	—	-181.07	225.36	—	—	-2258.53
15	—	31.43	-1.34	126.25	—	—	-860.36
16	—	68.97	15.98	48.7	—	—	-138.33
17	—	35.42	-41.9	73.86	-12.37	—	—
18	-17.42	11.72	15.12	53	—	—	—
19	16.6	—	0	138.64	—	—	-900.31
20	—	47.16	0	99.03	-7.43	—	—
21	—	105.03	2.3	64	—	-23.74	—
22	—	86.87	15.36	83.84	—	—	-454.69
23	-25.98	—	-10	165.68	—	—	-998.12
24	9.35	13.03	-10.7	13.65	—	—	—
25	-35	-29.7	42.43	59.5	—	—	—
26	—	25.52	-15.12	48.16	13.78	—	—
27	—	-48.7	-7.43	124	—	178.9	—
28	—	59.8	35.36	2.85	-51.96	—	—
29	-35	143.4	-42.43	7.65	—	—	—
30	-310.47	132.49	325.82	-97.77	—	—	—